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Solitary and compact-like shear waves in the bulk of solids

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We show that a model proposed by Rubin, Rosenau, and Gottlieb [J. Appl. Phys. 77 (1995) 4054], for dispersion caused by an inherent material characteristic length, belongs to the class of simple materials. Therefore, it is possible to generalize the idea of Rubin, Rosenau, and Gottlieb to include a wide range of material models, from nonlinear elasticity to turbulence. Using this insight, we are able to fine-tune nonlinear and dispersive effects in the theory of nonlinear elasticity in order to generate pulse solitary waves and also bulk travelling waves with compact support.

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The emergence of significant solitary waves from the equations governing the motion of solids requires usually a fine balance between nonlinearity and dispersion. The first ingredient finds its natural source in the theory of finite, fully nonlinear, elasticity, but the source for the second is more elusive. Often, specific boundary conditions (such as: a thin film coated on a substrate, the finite interface between phases in an elastic composite material, the lateral dimensions of a rod with free surfaces, etc.) are used because they introduce a characteristic length, to be compared with the wavelength. For homogeneous infinite (bulk) solids, the presence of a microstructure is invoked, recording the presence of inherent material characteristic lengths due to, for instance: the atomic lattice cells in a metal, the grain size in an alloy, the persistence and contour length in a polymer, etc. (it is worth noting that a similar situation also occurs in fluid dynamics, when inherent characteristic lengths may be not ignored in models of turbulence.) Although the standard constitutive equations of continuum mechanics can accommodate large strains and nonlinear material responses, they do not in general include the effects of characteristic material lengths [1]. The introduction of such information in models of material behavior is a subtle and difficult problem [2], and the modifications of the basic constitutive equations proposed in the literature are often unsatisfactory because they lead to physically unrealistic and mathematically ill-posed models [1, 2]. Finally, finding a simple connection between nonlinear and dispersive effects in material modeling is an interesting problem per se, because the balance between these two effects is at the origin of many fascinating phenomena, and in particular the propagation of solitons and compactons [4].

In 1987 Rosenau [2] proposed a regularized functional expansion of the equations for the dynamics of dense lattices in order to yield the leading effect of dispersion due to a characteristic length, via a physically reasonable and mathematically tractable differential equation. One of the advantages of this equation over other micro-mechanical or nonlocal approaches is that it models dispersion without increasing the number of initial or boundary conditions of the usual wave equation. On the same pathway, a three-dimensional phenomenological continuum model of the Rosenau approach was proposed by Rubin, Rosenau, and Gottlieb (RRG) in 1995 [3]. One aim of this Letter is to put in perspective that latter model by showing that it is a special case of the theory of simple materials in the sense of Noll [6], hence generalizing the original idea of Rosenau to a large class of material behavior, from nonlinear elasticity to fluid turbulence. Another objective is to find a clear and direct way to balance nonlinearity and dispersion in order to generate solitary waves with compact support in solids. This balance is attained by relying solely on constitutive arguments, without any resort to reductive asymptotic expansions; it is then compared (favorably, as it turns out) with the results obtained by such methods.

Let the motion of a body be described by a relation \( \mathbf{x} = \mathbf{x}(\mathbf{X}, t) \), where \( \mathbf{x} \) denotes the current coordinates of a point occupied by the particle of coordinates \( \mathbf{X} \) in the reference configuration at time \( t \). The deformation gradient \( \mathbf{F}(\mathbf{X}, t) \) and the spatial velocity gradient \( \mathbf{L}(\mathbf{X}, t) \) associated with the motion are defined by \( \mathbf{F} = \text{Grad} \mathbf{X} \) and \( \mathbf{L} = \text{grad} \mathbf{v} = (\mathbf{v} = \partial \mathbf{x}/\partial t) \), respectively (in this Letter, grad and div denote respectively the gradient and divergence operators with respect to the current position \( \mathbf{x} \), and Grad and Div denote the corresponding operators with respect to \( \mathbf{X} \).) The mathematical theory of simple materials is well-grounded from the mathematical and thermomechanical points of view [7]; there, the Cauchy stress \( \mathbf{T} \) is determined by the whole history of the deformation gradient,

\[
\mathbf{T} = \mathcal{G}_{\infty}^{\infty} \{ \mathbf{F}(t - s) \},
\]
where $\mathcal{G}$ is the constitutive functional. We now summarize the RRG model, which itself follows the axiomatic approach to continuum mechanics introduced by Green and Nagldi. Let us introduce the specific entropy per unit mass $\eta$, the specific rate of internal production of entropy $\xi$, the entropy flux per unit of present area $p$, and the specific Helmholtz free energy $\psi$. The set $\{\eta, \xi, p, \psi, T\}$ must satisfy, for all possible thermomechanical process, the restrictions coming from the balance of angular momentum, the energy equation, and from a suitable statement of the second law of thermodynamics. The central idea of Rubin et al. is to add terms $\{\psi_2, T_2\}$, modeling material dispersion, to the Cauchy stress tensor and the free energy: $T = T_1 + T_2$, $\psi = \psi_1 + \psi_2$, say, while the other quantities $\{\eta, \xi, \rho\}$ and the associated constitutive equations stay unchanged. They show that the balance of angular momentum and the energy equation then lead to $T_2 = T_2^T$ and

$$\rho\dot{\psi}_2 - T_2 \cdot D = 0, \quad (2)$$

respectively, where $\rho$ is the mass density per unit volume, a superposed dot denotes the material time derivative (at $X$ fixed), and $D = (L + L^T)/2$ is the stretching tensor. Further, the RRG model considers that $\psi_2$ is a single-valued function: $\psi_2 = \psi_2(\delta)$, where $\delta \equiv D \cdot D$ is an isotropic invariant; then from (2) follows that

$$T_2 = \rho\dot{\psi}_2(\delta) \left[ \text{grad} \ \dot{\psi} + (\text{grad} \ \dot{\psi})^T + 2L^T L - 4D^2 \right]. \quad (3)$$

Our first result is to show that $T_2$ is a special case of the Cauchy stress tensor associated with those non-Newtonian simple fluids denoted in the literature as second-grade fluids. Indeed, we have

$$\sigma = \nu A_1 + \alpha_1 A_2 + \alpha_2 A_2^T, \quad (4)$$

where $\nu$ is the classical Newtonian viscosity, $\alpha_1, \alpha_2$ are the microstructural coefficients (which may be taken as constants or as functions, for example of $\delta$), and the first two Rivlin-Ericksen tensors $A_1, A_2$ are defined by: $A_1 = 2D$, $A_2 = A_1 + A_1 L + L^T A_1$. Indeed, recall that $L = (\text{Grad} \ \dot{\psi}) F^{-1} = \hat{F} F^{-1}$, from which follows that

$$\dot{L} = (\text{Grad} \ \dot{\psi}) F^{-1} + LF(F^{-1}) = \text{grad} \ \dot{\psi} - L^2, \quad (5)$$

(where the last equality comes from the material time derivative of the identity $FF^{-1} = 1$). Substituting into $A_1 = L + L^T$ and into the definition of $A_2$, we find that the tensors $A_1$ and $A_2$ coincide when $\nu = 0$ and $\alpha_1(\geq 0) = -\alpha_2 = \rho \dot{\psi}_2$. We conclude that when $T_2$ is in the material class it is then the total Cauchy stress tensor $T = T_1 + T_2$ of the corresponding RRG model is also that of a simple material. This observation has many interesting consequences. For example, if $p$ is the Lagrange multiplier associated with the constraint of incompressibility (det $F = 1, \text{tr} \ D = 0$), then the classical choice of the Navier-Stokes stress tensor $T_1 = -\rho \mathbf{1} + \nu \mathbf{D}$ for the RRG model leads to those incompressible homogeneous fluids of second grade for which $\alpha_1 + \alpha_2 = 0$. We note that the equations of motion associated with those fluids, in the general and some special case, have been found to coincide with the equations derived by other means (asymptotic expansions, Lagrangian means, average Euler equation, etc.) in several models of turbulence and shallow water theory. Indeed, it is now clear that the presence of the RRG characteristic length is the reason of such connections.

Let us consider the case of the RRG model when $T_1$ corresponds to a hyperelastic, incompressible, isotropic solid, we have

$$T_1 = -\rho \mathbf{1} + 2(\partial \Sigma/\partial \mathbf{I}_1) B - 2(\partial \Sigma/\partial \mathbf{I}_2) B^{-1}. \quad (6)$$

Here $B = F F^T$, and $\Sigma = \Sigma(I_1, I_2)$ is the strain energy density, a function of the invariants $I_1 = \text{tr} \ B$ and $I_2 = \text{tr} \ B^{-1}$. Then the RRG model is a special case of the so-called solid of second grade. A rectilinear shearing motion is defined by

$$x = [X + u(Y, t)] e_1 + Y e_2 + Z e_3, \quad (7)$$

where $(e_1, e_2, e_3)$ is a fixed orthonormal triad. Then $B = 1 + u_1^T e_1 \otimes e_1 + u_Y (e_1 \otimes e_2 + e_2 \otimes e_1), B^{-1} = 1 + u_2^T e_2 \otimes e_2 - u_Y (e_1 \otimes e_2 + e_2 \otimes e_1), A_1 = u_Y (e_1 \otimes e_2 + e_2 \otimes e_1)$, and $A_2 = u_Y (e_1 \otimes e_2 + e_2 \otimes e_1) + 2u_1^T e_2 \otimes e_2$. Also, $I_1 = 2 = 3 + u_2^2$, and $\delta = \delta_2$. The equations of motion in the absence of body forces ($\text{div} \ T = \rho \dot{\psi}$) reduce to the three scalar equations:

$$-\partial p/\partial X + \partial T_{12}/\partial Y = \rho \partial^2 u/\partial t^2, \quad \partial T_{22}/\partial Y = 0, \quad -\partial p/\partial Z = 0, \quad (8)$$

for which we used (3), or its equivalent form: $T_2 = \rho \dot{\psi}_2(A_2 - A_2^T)$. The third equation gives $p = p(X, Y, t)$ and then the cross-differentiation of the first and second equations leads to $p(X, Y, t) = -2\Sigma_2 u_2^2 + \rho \dot{\psi}_2 u_2^2 + p_1(t)X + p_0(t)$, where $p_0, p_1$ are arbitrary functions of $t$ alone and $\Sigma_2$ is the partial derivative of $\Sigma$ with respect to $I_2$. We are left with a single determining equation for the displacement $u(Y, t)$: $p_1 + [2(\Sigma_1 + \Sigma_2) u_Y + \rho \dot{\psi}_2 u_Y u_Y] = p u_Y$, or, taking the derivative with respect to $Y$, a single equation for the strain $U \equiv u_Y$:

$$\left[ \bar{\mu} U + \beta U_{tt} \right]_{YY} = \rho U_{tt}, \quad \bar{\mu} = 2(\Sigma_1 + \Sigma_2), \quad \beta = \rho \dot{\psi}_2. \quad (9)$$

Here $\mu = \mu(U^2) > 0$ is the generalized shear modulus of nonlinear elasticity; it is a constant (Lamé’s second constant) in linear elasticity, and also in nonlinear elasticity for the special cases of the neo-Hookean (“geometric” nonlinearity) and of the Mooney-Rivlin (“geometric” and “physical” nonlinearities) forms of the strain energy $W = C_{10}(I_1 - 3), C_{10}(I_1 - 3) + C_{01}(I_2 - 3)$, respectively). However in general, a nonlinear constitutive equation for the solid yields a non-constant $\mu$; similarly,
a general dispersive material behavior is attested by a non-constant function $\beta = \beta(U_0^2) > 0$ (the case where $\hat{\mu}$ and $\hat{\beta}$ are both constants is considered elsewhere \cite{12}). To illustrate some features of the RRG model, we make the following constitutive choices: $\hat{\mu}(U_0^2) = \mu_0 + \mu_1 U_0^2$ and $\hat{\alpha}(U_0^2) = \rho(\beta_0 + \beta_1 U_0^2)$, where $\mu_0 > 0$ is the infinitesimal shear modulus of the solid. We seek a travelling wave solution: $U = V(\xi)$, $\xi = Y - ct$, with drop boundary conditions: $V^{(n)}(\pm \infty) = 0$, $n \geq 0$. Then successive integrations of the reduced governing equation lead to
\begin{equation}
\rho c^2 \beta_1 (V')^4 + 2\rho c^2 \beta_0 (V')^2 + [\mu_1 V^2 - 2(\rho c^2 - \mu_0)] V^2 = 0.
\end{equation}

(10)

For a linear variation of the dispersion free energy $\psi_2$ with the isotropic invariant $\gamma = D \cdot D$, we have $\beta_1 = 0$ and the following solitary wave solution:
\begin{equation}
V(\xi) = \sqrt{\frac{2 \rho c^2 - \mu_0}{\mu_1}} \operatorname{sech} \sqrt{\frac{\rho c^2 - \mu_0}{\rho c^2} \frac{\xi - \xi_0}{\sqrt{\beta_0}}},
\end{equation}

(11)

where $\xi_0$ is arbitrary. This wave is supersonic with respect to the speed of an infinitesimal shear wave but $c$ is otherwise arbitrary. Figure 1 shows its profile for several values of $\rho c^2/\mu_0$.

Now, we know from previous results \cite{15} that \cite{10} has no compact-like solutions when $\beta_0 \beta_1 \neq 0$. On the other hand, when $\beta_0 = 0$, $\beta_1 \neq 0$, it is of the form
\begin{equation}
(V')^4 = (\gamma_0 - \gamma_1 V^2)V^2,
\end{equation}

(12)

(where $\gamma_0 = 2(\rho c^2 - \mu_0)/(\rho c^3 \beta_1)$ and $\gamma_1 = \mu_1/(\rho c^4 \beta_1)$), the right hand-side of which has a double zero (at $V = 0$) and two simple zeros (at $V = \pm \sqrt{\gamma_0/\gamma_1}$). This observation alone is sufficient to conclude that \cite{12} admits a compact wave solution. As it happens, these can be integrated in terms of special functions. Indeed, introducing the hypergeometric function $\operatorname{Hyp}_2 F_1(a,b,c,z)$, solution to the second-order linear differential equation $z(1-z)y'' + [c - (a + b + 1)z]y' - aby = 0$, we find the following identity,
\begin{equation}
\int (u^2 - u^4)^{-1/4} du = 2(u^2)^{1/4} \operatorname{Hyp}_2 F_1 \left[ \frac{1}{4}, \frac{1}{4}, \frac{5}{4}, u^2 \right].
\end{equation}

(13)

We call $I(u)$ that function and observe that it is defined on the interval $0 \leq u \leq \pi/\sqrt{2}$, where it increases in a monotone way from 0 to 1. Then we manipulate \cite{12} to give
\begin{equation}
\sqrt{\gamma_1/\gamma_0} V(\xi) = I^{-1}(\gamma_1^{1/4}(\xi - \xi_0)),
\end{equation}

(14)

where $\xi_0$ is arbitrary. Hence we can build a weak solution with finite support measure $\sqrt{2\pi \gamma_1^{-1/4}}$, defined by:
\begin{equation}
\sqrt{\gamma_1/\gamma_0} V(\xi) = I^{-1}(\gamma_1^{1/4}) \quad \text{on } [0, \pi/a],
\end{equation}

(15)

$$= I^{-1}(\gamma_1^{1/4}(\sqrt{2\pi} - \xi)) \quad \text{on } [\pi/a, \sqrt{2\pi}/a],$$

and zero everywhere else, see Figure 2. (Here $a = (4 \gamma_1)^{1/4}$. This wave shares some characteristics with the solitary wave \cite{11}: it is supersonic, its amplitude is proportional to $\sqrt{\gamma_0/\gamma_1} = \sqrt{2(\rho c^2 - \mu_0)/\mu_1}$, growing with the speed; in contrast, its width evolves as $\gamma_1^{-1/4}$, which is proportional to $c$. We emphasize that this compact wave is derived solely on the basis of constitutive arguments, by taking the generalized shear modulus $\hat{\mu}$ linear in the squared shear (nonlinear effect) and the free energy density $\psi_2$ proportional to $\delta^2$ (dispersive effect). Previous attempts at finding compact waves relied on ad hoc asymptotic reductive approaches \cite{16} and to the best of our knowledge, a bulk compact wave has never been generated in the framework of nonlinear elasticity \cite{1} p. 91]

Finally we look at reductive asymptotic expansions of the strain equation of motion \cite{4}. We consider that the generalized shear modulus is slightly nonlinear, $\hat{\mu} = \mu_0 + (1 + \epsilon U_0^2)$ where $\epsilon$ is a small parameter, and that the dispersion is also of order $\epsilon$: for instance, when $\psi_2$ is linear in $\beta$, we take: $\beta = 2(\rho a^2)\epsilon$, where $a$ is a constant with the dimensions of a length. With the stan-
In conclusion, we believe that this investigation demonstrates the usefulness, the versatility, and ultimately the beauty of the RRG model. Although the RRG model originates from a microstructural model [3], it can now be apprehended as a purely phenomenological approach to dispersion, applicable to the whole class of simple materials. It overcomes the usual problems of nonlocal theories, it unifies several results in the literature, and it provides a natural and detailed study of localization of traveling waves in elastic materials. Yet several topics raised here merit further scrutiny: is the solitary wave exhibited a soliton? is the compact wave a compacton? Also, the analysis relied on specific constitutive equations. Hence for the nonlinear elasticity, the generalized shear modulus was that of a solid having strain energy density in the form \[ \Sigma = C_{10}J_1 + C_{01}J_2 + C_{20}J_1^2 + C_{11}J_1J_2 + C_{02}J_2^2 \]

where \( J_1 = I_1 - 3 \) and \( J_2 = I_2 - 3 \) (so that \( \mu_0 = 2(C_{10} + C_{01}) \) and \( \mu_1 = 4(C_{20} + C_{11} + C_{02}) \)). Although this, and higher-order, truncation of the polynomial expansion of \( \Sigma \) are highly popular in experimental nonlinear elasticity, in curve fitting, and in finite element packages, it should be acknowledged that the determination of the “best” \( C_{ij} \) is a messy procedure [21]. Eventually, it might be of greater (and safer) interest to consider other types of nonlinear strain energy densities, such as those arising in biological soft tissues, which incorporate the effect of strain hardening. Similar remarks hold for the nonlinear dispersion, for which the free energy was taken as \( \psi_2 = \alpha_0 \delta + (\alpha_1/2) \delta^2 \).

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