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Effect of fast pyrolysis conditions on biomass solid residues at high temperatures

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Abstract

Fast pyrolysis of wood and straw was conducted in a drop tube furnace (DTF) and compared with corresponding data from a wire mesh reactor (WMR) to study the influence of temperature (1000-1400)°C, biomass origin (pinewood, beechwood, wheat straw, alfalfa straw), and heating rate (10³°C/s, 10⁴°C/s) on the char yield and morphology. Scanning electron microscopy (SEM), elemental analysis, and ash compositional analysis were applied to characterize the effect of operational conditions on the solid residues (char, soot) and gaseous products. The char yield from fast pyrolysis in the DTF setup was 3 to 7% (daf) points lower than in the WMR. During fast pyrolysis pinewood underwent drastic morphological transformations, whereas beechwood and straw samples retained the original porous structure of the parental fuel with slight melting on the surface. The particle size of Danish wheat straw char decreased in its half-width with respect to the parental fuel, whereas

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the alfalfa straw char particle size remained unaltered at higher temperatures. Soot particles in a range from 60 to 300 nm were obtained during fast pyrolysis. The soot yield from herbaceous fuels was lower than from wood samples, possibly due to differences in the content of lignin and resin acids.

Keywords: fast pyrolysis, drop tube furnace, wire mesh reactor, soot, CAMSIZER XT

1. Introduction

Suspension firing of biomass is widely used for power generation and has been considered as an important step in reduction of greenhouse gas emissions. Unlike coal, biomass is difficult to mill to $< 100 \mu\text{m}$ due to its fibrous structure, resulting in higher energy consumption for the comminution process. The shape and size distribution of ground biomass particles consists of a larger fraction of flake- and cylinder-like particles with a particle size $> 300 \mu\text{m}$. In biomass suspension firing, it is a challenge to achieve high fuel conversion at the short residence time while minimizing the input for milling. This is further challenged by application of a broad biofuel range to obtain high operational flexibility at power plants. Thus an increased energy input into the biomass comminution process affects the total efficiency of a power plant, and large particle sizes may cause problems with flame stability and burnout.

In suspension firing, biomass particles are heated rapidly to high temperatures of 1000-1400°C, leading to volatile release and formation of solid residues (char and soot) during devolatilization. The solid residue yield and its properties, including particle size and shape, composition, reactivity and

19 burnout, depend strongly on the operational conditions of fast devolatiliza-
20 tion [1–4]. A number of studies [5–11] have investigated structural changes of
21 different biomass types and their plant cell components during fast pyroly-
22 sis. Sharma et al. [5–7, 12] reported structural changes of lignin and tobacco
23 char at temperatures up to 750°C with rapid heating rates, accompanied by
24 softening and melting of a solid phase. The effect of char plasticization was
25 observed mostly at high heating rate of pyrolysis ($> 10^3$ °C/s) [8, 9, 13–15].
26 The char fluidity of coal and lignin during pyrolysis was described by the
27 FG-DVC model (Functional Group - Depolymerization, Vaporization and
28 Cross-linking model) of Solomon et al. [16, 17]. They pointed out that the
29 char fluidity is influenced by small differences in the cross-linking rate with
30 oxygen, affecting cross-linking and preventing char fluidity [18].

31 Previous investigations of biomass pyrolysis [9, 15, 19, 20] ascribed the
32 char structural transformations and changes in reactivity to the catalytic
33 effect of minerals (K, Ca, Mg and Si). Wornat et al. [19] reported migration
34 of alkali and alkaline earth metals to the particle surface for high oxygen
35 content fuels, with the formation of beads on the char shell, accompanied by
36 a highly cross-linked carbon structure that hindered crystallite mobility and
37 graphitization during combustion. Dall’Ora et al. [9] studied fast pyrolysis
38 of beechwood in an entrained-flow reactor, and concluded that calcium and
39 potassium catalyze cross-linking, resulting in a higher char yield and less
40 severe char morphological changes.

41 In the present study the relation between different types of biomass and
42 their solid residue (char, soot) properties was investigated. Char and soot
43 yields were obtained from fast pyrolysis in a drop tube furnace (DTF). The

44 char yields from the DTF were compared with results from a wire mesh reac-
45 tor (WMR) [21] at temperatures $> 1000^{\circ}\text{C}$ to study the simultaneous effect
46 of temperature, heating rate, and biomass origin on the char yield. The in-
47 fluence of extractives on the structural changes, on which available literature
48 is not extensive, was also studied using char from the DTF. This work also
49 attempted to fill a gap about the effect of biomass origin on the soot forma-
50 tion during fast pyrolysis. The influence of ash composition, particularly of
51 K and Ca elements, on the char morphological changes under fast heating
52 was characterized by SEM and TEM microscopy.

53 **2. Materials and methods**

54 *2.1. Original biomass characterization*

55 Pinewood, beechwood, Danish wheat straw, and alfalfa straw were se-
56 lected for the fast pyrolysis study in the DTF and WMR. The wheat straw
57 was leached in deionized water (room temperature) by continuous stirring
58 for 12 hours, followed by drying at 30°C in an oven desiccator without any
59 ventilation. The mineral content after biomass leaching was determined by
60 ash analysis. Due to the wheat straw leaching, the metal content was re-
61 duced to $\approx 60\%$ of the original value and the Cl, S, K, Na and P contents
62 were strongly reduced [21]. The leached wheat straw was selected to study
63 the influence of alkali on the char and soot yields.

64 The proximate and ultimate analyses of fuels are shown in Table 1. The
65 fuels were milled on a Retsch rotor mill RZ200 and sieved to a particle size
66 fraction of 0.2-0.425 mm. The wood and herbaceous fuels were selected for
67 the present study, based on the differences in organic and inorganic matter.

68 The compositional analysis of biomass (cellulose, hemicellulose, acid-soluble
69 lignin, acid-insoluble lignin, protein and extractives) was conducted accord-
70 ing to NREL technical reports [22–24] and Thammasouk et al. [25], and shown
71 in Table 2.

72 The water-ethanol extraction was performed on wheat straw and alfalfa
73 straw which contain a high level of hydrophilic and lipophilic extractable
74 compounds as described by Thammasouk et al. [25]. Extraction with acetone
75 on pinewood and beechwood was done for the quantitative estimation of
76 extractives in the original biomass, and to remove resin and fatty acids,
77 waxes, and phytosterols for the investigation of char structural changes under
78 fast heating as described in the supplemental material.

79 *2.2. Experimental apparatus and procedure*

80 *2.2.1. Drop Tube Furnace*

81 The Drop Tube Furnace (DTF) used in the present study is shown in
82 Figure 1. The cylindrical reactor tube was made of alumina ceramic (grade
83 C799) with an inner diameter of 54 mm. The reactor tube was heated by tube
84 furnace modules using SiC rods as heating elements (Elite Thermal Systems
85 Ltd.) with a maximum temperature of 1500°C. Supply of primary gas was
86 led through the biomass feeder, and secondary gas was led to the top of the
87 reactor through a packed bed of ceramic balls that distributed the gas flow
88 equally in the radial direction. Inlet gas flows of O₂, N₂, H₂, CO and CO₂
89 were controlled by mass flow controllers (EL-FLOW[®] Select, Bronkhorst
90 High-Tech B.V.), while the flow rate of H₂O was controlled by a syringe
91 pump (Legato 100, KD Scientific Inc.). A syringe pump type biomass feeder

92 was used to supply biomass at low feeding rates [26]. The feeding probe was
93 water-cooled at 20°C to ensure a high heating rate of the biomass when it
94 entered the reactor. The Reynolds number of the gas flow inside the reactor
95 was 60-100, dependent on the reaction temperature.

96 Biomass was rapidly heated and reacted while it fell down through the
97 reactor. Reaction products were separated into coarse particles (mainly char
98 and fly ashes), fine particles (mainly soot and precipitated ash vapor), and
99 permanent gases. Soot particles passing the cyclone (cut size 2.5 μm) were
100 captured from the product gas flow by a grade QM-A quartz filter with a
101 diameter of 50 mm (Whatman, GE Healthcare Life Science). The larger
102 particles (e.g. char) could either fall down to a char bin or a stainless steel
103 cyclone with cut size of 2.5 μm (URG-2000-30ENS-1, URG Corporation).
104 After an activated carbon filter (VACU-GUARD 150, GE Healthcare Life
105 Science), the gas composition was measured by a micro gas chromatograph
106 (Model 490, Agilent Technologies). The μGC was equipped with two columns
107 (CP-MolSieve 5 A for H_2 , O_2 , N_2 , CH_4 and CO ; and PoraPlot U for CO_2 ,
108 C_2H_4 , C_2H_6 , C_2H_2 , and $\text{C}_3\text{H}_6/\text{C}_3\text{H}_8$) and thermal conductivity detectors.
109 The temperature of the char bin and product gas was controlled by heating
110 controllers (HTC-5500, Hemi Heating AB) with thermo-tapes (S-type, Hemi
111 Heating AB) and kept at 200°C to avoid tar condensation.

112 In the present study, the experiments were conducted by feeding ≈ 5 g
113 of biomass at a rate of 0.2 g/min. Both primary and secondary gases were
114 N_2 , and the flow rate of primary gas was 180 mL/min and that of secondary
115 gas was 4.8 L/min. The residence time of the fuel particles was estimated
116 to be about 1 s, taking into account the density change during pyrolysis [11].

117 Three reaction temperatures (1000, 1250 and 1400°C) were applied.

118 2.2.2. *Wire mesh reactor*

119 The wire mesh reactor at TU Munich used in this study was previously
120 described by Tremel et al. [27]. A schematic drawing is shown in the supple-
121 mental material (Figure S-2). It could be operated up to a temperature of
122 1700°C, at a heating rate of 5000°C/s, and a maximal pressure of 50 bar.

123 2.2.3. *Measurement uncertainty*

124 For the DTF, the measurement error was calculated for each component
125 of a mass balance (C_xH_y +vapor, gas, coke, soot). The absolute extended
126 uncertainty of the product yield was determined by a Gaussian error prop-
127 agation procedure [28], based on the equations shown in the supplemental
128 material (S-4). The average standard measurement error in the present study
129 was ± 2 wt. %, within a 95 % confidence interval for the DTF experiments.
130 The volatile measurements with a micro gas chromatograph and soot loss
131 in the DTF setup were sources of experimental error (< 15 %) as shown in
132 the calculated carbon / hydrogen balances. Another source of error was the
133 non-measured fractions of vapor, tars and larger hydrocarbons in the DTF.

134 For the WMR, the error bars represent the standard deviation from the
135 mean of the series of experiments at each condition [21]. The char yield data
136 obtained in the wire mesh reactor were plotted as a representative average of
137 at least five experiments. The measurement uncertainties of the char yields,
138 prepared in the WMR, were < 6 %. The inaccuracy in determining the char
139 yield was mainly caused by weighting errors.

140 *2.2.4. Solid residue characterization*

141 Three different solid residues were distinguished in the present study,
142 namely char, soot and coke. Char and soot were collected in a char bin
143 and on a filter at the different experimental temperatures. Char is the frac-
144 tion of non-devolatilized solid from the initial biomass, consisting mainly of
145 carbon and ash with minor presence of hydrogen and oxygen. Coke, the car-
146 bonaceous material deposited on the reactor walls, was quantified after each
147 experiment by measurement of the concentration of CO₂ during oxidation.

148 *SEM and TEM microscopy.* SEM analysis of char was performed on a micro-
149 scope (FEI Company, Inspect) with a tungsten filament under high vacuum
150 in order to understand char structural and chemical properties. Prior to the
151 analysis, char samples were coated with a thin layer of carbon (40 sec, 5 mA)
152 using a Cressington 208 Carbon Coater to avoid sample charging.

153 Soot samples were studied on the transmission electron microscope (200-
154 kV FEI Tecnai T20 G²). Prior to the microscopy, soot samples were kept at
155 350°C for 4 hours in a thermo-gravimetric instrument (TGA) to reduce the
156 amount of volatiles. The TGA curves shown in the supplemental material
157 (Figure S-7) quantified the remaining volatiles yield to be < 5%. TEM
158 analysis of soot was performed using dry method to avoid nano-structure
159 changes as shown in the supplemental material (Figure S-8). In addition,
160 soot samples were grounded a very short time using a pestle and mortar, to
161 ensure homogeneous particle distribution, and placed on a Cu grid. Imaging
162 of soot samples was performed in vacuum using a Gatan 894 2K UltraScan
163 1000 CCD camera and a FEI single-tilt holder.

164 *Elemental analysis.* The elemental analysis was performed on two instru-
165 ments of the same model (Eurovector, model EA3000). Acetanilide was used
166 as a reference standard. The ash content was determined using a standard
167 ash test at 550°C, according to the procedure described in DIN EN 14775.

168 *Ash compositional analysis.* The ash compositional analysis was performed
169 by an X-ray fluorescence instrument (Shimadzu, model EDX 800-HS) at TU
170 Munich. Prior to the XRF analysis, char samples were pre-heated in oxygen
171 at 5°C/min up to 550°C and kept at that temperature for 7 h. The generated
172 ash (about 200 mg) was initially mixed and then pressed with a special wax
173 (mixture ratio 1:5). The Cl and S content in the ash was analyzed by ICP-
174 OES/IC at TU Wien. The ash sample was dissolved in ultrapure water
175 at 120°C for 1 h, and then the solution was filtered and analyzed by ICP-
176 OES/IC.

177 *Particle size and shape.* The particle size and shape of the original biomass
178 and its char were characterized on a 2D dynamic imaging instrument (CAM-
179 SIZER XT, Retsch), designed for a particle size range of 3 μm to 3 mm. A
180 particle shadow was captured by the CCD-basic and zoom cameras of the
181 CAMSIZER XT. The zoom-camera was optimized to analyze smaller parti-
182 cles with a high resolution, whereas the basic-camera detected larger particles
183 due to a large field of view. The projected area of a particle was analyzed by
184 the CAMSIZER XT 6.3.10 software to characterize its size and shape. Fine
185 biomass particles tended to agglomerate which made it difficult to detect the
186 true geometric dimensions of each individual particle. Therefore, the par-
187 ticle agglomerates were separated without destroying the primary particles

188 by air pressure dispersion. For the particle size analysis, ca. 100 mg of sam-
189 ple was used. The particle size and shape measurements of char, collected
190 from several drop tube pyrolysis experiments, were performed twice with
191 the CAMSIZER XT for each operational condition to establish reproducible
192 results.

193 The Martin minimal ($x_{Ma,min}$) and Feret maximal ($x_{Fe,max}$) diameters
194 are suitable parameters to represent the biomass particle width and length
195 in combustion. The Martin diameter is a chord length that divides the pro-
196 jected particle area into two equal halves [29], as shown in the supplemental
197 material (Figure S-5). The minimal Martin diameter ($x_{Ma,min}$) is determined
198 from the smallest Martin diameter of the particle projection [30], and rep-
199 represents a particle width based on the assumption of a biomass particle to
200 be thinner than its width in the diffusion process in combustion. The Feret
201 diameter is the distance between two tangents placed perpendicular to the
202 measurement direction [29], as shown in the supplemental material (Figure
203 S-5). The Feret maximal diameter is applied as the largest value of all mea-
204 sured Feret diameters of a particle [30], and the longest measurable diameter
205 $x_{Fe,max}$ is the largest diameter to fulfill the assumption that the length of
206 a particle has to be larger than its width. The results of the particle size
207 analysis were represented as a frequency distribution over $x_{Ma,min}$, as defined
208 in equation 1:

$$q_3(x_{Ma,min}) = \frac{dQ_3(x_{Ma,min})}{x(x_{Ma,min})} \quad (1)$$

209 where Q_3 is the cumulative particle size distribution based on volume. The
210 particle shape was characterized by sphericity (SPHT) and aspect ratio (b/l)
211 in the present study. Sphericity is one of the most common ways to express

212 the deviation of an 2D image shape from a sphere and is defined by equation 2:

$$SPHT = \frac{4 * \pi * A}{P^2} \quad (2)$$

213 where P is the measured circumference of a particle projection and A is
214 the measured area of a particle projection. The particle is considered to be
215 spherical when the value of sphericity is equal to one and non-spherical when
216 it is smaller than one. The aspect ratio (AR) is defined as the ratio of particle
217 width ($b = x_{Ma,min}$) to the particle length ($l = x_{Fe,max}$).

$$AR = \frac{b}{l} \quad (3)$$

218 **3. Results and discussion**

219 *3.1. Carbon and hydrogen balances*

220 The mass balances of the DTF experiments with respect to measured
221 solid residues (char, soot, coke) and major gaseous products (CO_2 , H_2 , CO ,
222 CH_4 , C_3H_8 , C_2H_4 , C_2H_2) in dependency on the heat treatment temperature
223 are shown in Figure 2. The amount of vapor, tars, and larger hydrocarbons
224 was not measured in the present study, but estimated by difference from the
225 mass balance. The carbon and hydrogen balances represent an average of at
226 least two measurements. During fast pyrolysis, mainly gaseous products were
227 formed, along with lower amounts of solid residues at higher temperatures.

228 At 1000°C , the yield of larger hydrocarbons and vapor was significantly
229 larger than at higher temperatures. The carbon in wood and herbaceous
230 biomasses was converted to gas, soot and char. Hydrogen was present mostly
231 in gaseous products, tars, larger hydrocarbons and vapor at 1000°C . Almost

232 all hydrogen ($> 90\%$) was found in the form of gaseous products above
233 1250°C for wood and herbaceous biomasses. Higher temperatures suppressed
234 tar formation and enhanced hydrogen and oxygen release to gaseous prod-
235 ucts.

236 *3.2. The solid product yield*

237 *Char yield.* The wire mesh reactor (WMR) results were obtained by Trubet-
238 skaya et al. [21]. In that study, the char yield (daf) was represented including
239 inorganic matter in char relative to the biomass on dry and ash-free basis.
240 In the present work, char yields of wood and herbaceous biomass in both
241 reactors are shown on dry ash free basis (daf), excluding inorganic matter in
242 char relative to original biomass (daf) in Figure 3. The biomass char yield
243 at fast pyrolysis conditions depends strongly on the biomass origin, tem-
244 perature and heating rate. Straw (herbaceous) samples showed higher char
245 yields compared with wood and leached wheat straw due to the presence of
246 alkali metals as known from the literature [15, 19, 20, 31]. The char yields
247 of pinewood and beechwood showed significant differences, possibly due to
248 differences in lignin content, presence of temperature stable extractives, and
249 alkali metal content (higher in beechwood).

250 As a general trend, the char yield of beechwood, wheat straw and alfalfa
251 straw decreased with increasing temperature, indicating a dependency of the
252 char yield on the heat treatment temperature. On the other hand, the char
253 yield of pinewood and leached wheat straw decreased only slightly between
254 1000 and 1400°C , being lower than the char yield of other fuels at 1000°C .
255 The continuous decrease in char yield from wheat straw (rich in K, Si) and
256 alfalfa straw (rich in Ca, K) was attributed partly to high-temperature ash

257 reactions, leading to the volatile ash release, and affecting the organic matter
258 release. The results indicate that the influence of alkali on the char yield is
259 more pronounced at low and intermediate heating rates than at fast heating
260 rates in the DTF as shown in Figure S-11.

261 The results showed that there is a clear difference between char yields
262 in the WMR and DTF. The char yield in the DTF was 3-7 % wt. (daf) lower
263 than that in the WMR, possibly due to the differences in heating rate and
264 residence time. The pyrolysis in the WMR was carried out with a lower
265 heating rate (1000°C/s) than in the DTF (10⁴-10⁵°C/s). When the holding
266 time in the WMR was increased from 1 to 2 s, the char yield became slightly
267 lower [21].

268 *Soot yield.* Figure 4 shows the soot and char yields, each separated into or-
269 ganic matter and ash. The soot yield varied between different biomasses at
270 similar operational conditions. The highest soot yield was observed during
271 pinewood fast pyrolysis. The soot yield increased with temperature, reach-
272 ing a peak value at 1250°C, and slightly decreased at higher temperatures,
273 corresponding to the well-known soot yield curvature [32].

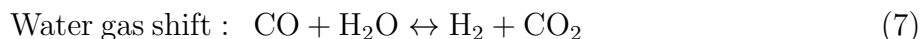
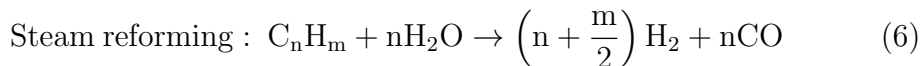
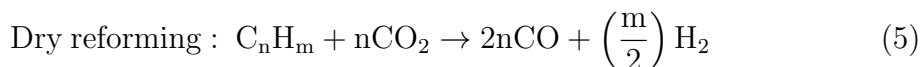
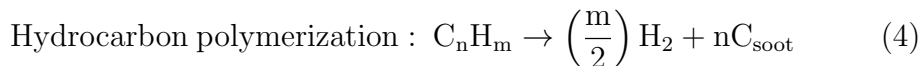
274 Figure 4 shows large differences in the soot yield of wood, leached wheat
275 straw and herbaceous biomass. The fact that beechwood and leached wheat
276 straw exhibit major differences in soot yield despite similar alkali (i.e. K⁺)
277 and holocellulose contents indicate that these parameters are of minor im-
278 portance for the soot fraction. Instead, lignin and extractives in the original
279 biomass possibly are important for the soot yield. The leaching of alkali from
280 wheat straw resulted in a removal of lignin and other organic compounds as
281 shown in Table 2, leading to the decreased formation of PAH precursors, and

282 thereby to lower soot yields. Williams et al. [33] suggested that biomass with
283 a high content of lignin may form larger soot fractions due to its ability to
284 generate phenolic tars. A significant fraction of aromatic tars and soot orig-
285 inates from lignin pyrolysis, mainly composed of guaiacol and syringol-type
286 units [34–36]. Ross et al. [37] stated that wood soot contains PAH material,
287 promoted by the presence of acetylene at higher temperatures. The sug-
288 gestion is consistent with the gas measurement results of the present study.
289 The measured C_2H_2 concentration is up to 0.05 vol. % in inert nitrogen dur-
290 ing fast pyrolysis of wood and herbaceous biomasses at $1000^\circ C$ shown in
291 Figure 5. With increasing temperature, the C_2H_2 yield decreased, whereas
292 the soot yield increased. Moreover, C_2H_4 might affect the soot yield at high
293 temperatures, facilitating PAH molecule growth [37]. The high concentra-
294 tion of resin acids in pinewood could increase the soot yield in addition to a
295 stronger formation of PAH precursors [38, 39].

296 *3.3. Volatile gas composition*

297 The concentrations of H_2 , CO , CO_2 and C_xH_y (CH_4 , C_2H_2 , C_2H_4) are
298 shown in Figure 5. The gas composition changed significantly with increas-
299 ing heat treatment temperature. Higher temperatures favor cracking of the
300 volatile hydrocarbon products, increasing the yield of H_2 generated mainly
301 from dehydrogenation. Soot formation could lead to increase in the yields
302 of H_2 and CO between 1000 and $1250^\circ C$ due to polymerization and dry

303 reforming reactions, equations 4 and 5.



304 The yield of CO_2 decreased and those of CO and H_2 increased for all biomass
305 at temperatures above $1250^\circ C$ due to dry (equation 5) and steam reforming
306 (equation 6) and the water-gas shift reactions (equation 7).

307 In the literature [40–43], the larger fractions of H_2 and CO and a lower
308 fraction of CO_2 along with lower yields of char were related to self-gasification
309 in a drop tube reactor. However, according to calculations (see Table S-
310 1) the self-gasification reaction is slow under the present conditions. The
311 differences observed in the char yields between the WMR and DTF were
312 mainly attributed to changes in heating rate and not self-gasification.

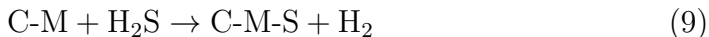
313 3.4. Alkali transformations of herbaceous biomasses

314 *Char alkali.* The weight of each inorganic element retained in alfalfa and
315 wheat straw char from DTF is shown in Figure 6, based on the original
316 sample weight. The main difference between the composition of the two
317 fuels was the ash content, which was higher (7.2 %) in alfalfa straw than in
318 wheat straw (4.1 %). Wheat straw char contained predominantly Si, K and
319 Ca elements, whereas the alfalfa straw char mostly consisted of Ca, K, S, Si,
320 P and Mg. The original alfalfa straw was characterized by a high level of K
321 and Ca, and therefore forming mainly K and Ca rich compounds in the char.

322 The inorganic composition of original wheat straw showed a large frac-
323 tion of Si (seven times larger than in alfalfa straw), leading to the formation
324 of silicates during devolatilization. Thermodynamic equilibrium calculations
325 of gas and solid phases, performed with the Factsage software, indicated that
326 under reducing conditions potassium in the alfalfa and wheat straw chars was
327 most likely present as chlorides and silicates. In addition, potassium and cal-
328 cium could be present as carbides in the alfalfa straw. In the wheat straw
329 char, calcium was obtained as a silicate.

330 *Soot inorganic content.* The beechwood and straw soot clusters contained
331 both organic matter and minerals as shown in Figure 7. The mineral com-
332 pounds in the soot arose from the condensation of inorganic species from the
333 gas phase onto the soot. It appeared that the inorganic elements in alfalfa
334 and wheat straw soot mainly consisted of K, Cl and S. The high levels of K
335 and Cl in the soot matter was probably caused by the KCl release under fast
336 heating in the DTF.

337 As it can be seen in Figure 7, a high level of sulfur (about 0.8 wt. %) was
338 observed in both soot samples. The Factsage equilibrium calculation showed
339 that sulfur was most likely released as H₂S gas, in agreement with literature
340 results [44, 45]. Hydrogen sulfide could possibly react with soot active sites
341 or with metals, as shown by Cal et al. [46]:



342 *3.5. Solid residue characterization*

343 *3.5.1. Particle size and shape analysis of char*

344 The particle size and shape of the original biomass and its char were
345 analyzed by CAMSIZER XT instrument. Prior to the 2D dynamic imaging
346 analysis, the original fuel was sieved to a particle size fraction of 0.2-0.4 mm.
347 As shown in Figures 8 and 9, the results of the particle characterization study
348 indicate nearly 50 % decrease of the characteristic length of pinewood, beech-
349 wood and wheat straw during pyrolysis in comparison to the original fuel,
350 while further changes in particle size between 1000 and 1400°C are almost
351 negligible. The particle size of alfalfa straw char remained similar to the
352 original fuel at heat treatment temperatures of 1000-1400°C. This may be
353 attributed to formation of calcium carbonates and silicates (as shown by
354 the Factsage simulation), which form a very stable inorganic matter shell,
355 hindering particle shrinkage.

356 The particle shape of biomass was characterized using the sphericity
357 (SPHT) and width/length ratio (b/l) parameters. The pinewood char par-
358 ticles showed a near-spherical shape (SPHT = 0.8-0.9; b/l = 0.7-0.8). The
359 beechwood and herbaceous chars obtained cylindrical or rectangular shapes
360 (SPHT = 0.5-0.8; b/l ratios = 0.4-0.7). The results of particles > 0.4 mm in
361 terms of shape description were considered as non-representative due to the
362 low presence of particles in this fraction. It seems that at high heating rates
363 in the DTF (about 10⁴°C/s), a biomass particle transforms to one particular
364 shape that stays unchanged with increasing temperature above 1000°C.

365 *3.5.2. Char and soot structure*

366 *Char morphology.* Figure 10 shows SEM images of wood and herbaceous
367 char, pyrolyzed at 1000 and 1400°C in the drop tube reactor. The wood
368 and herbaceous char particles have undergone softening and melting. At
369 higher temperatures, the char plasticization is attributed to the formation
370 of liquid metaplast due to the depolymerization with subsequent repolymer-
371 ization and cross-linking, leading to char formation [47]. The differences in
372 cross-linking propensity influence the fluidity of char significantly. The for-
373 mation of metaplast depends on the complex interaction of all plant cell
374 compounds (holocelluloses, lignin and extractives). Heating rates affect the
375 melting and swelling behavior of biomass, since the relative rates of compet-
376 ing processes for tar formation (bond-breaking, cross-linking, internal mass
377 transport) change with the temperature. The heating rates determine the
378 temperature at which reaction occurs [48], leading at high heating rates to
379 a significant bridge-breaking in biomass before it starts to cross-link and
380 therefore becomes fluid. On one hand, the inorganic matter could conceiv-
381 ably influence the char morphology since potassium and calcium may act as
382 active catalysts, affecting the metaplast formation. On the other hand, the
383 inorganic matter probably does not have sufficient time to affect cross-linking
384 due to the fast bonds breaking at very high heating rates.

385 The SEM images showed that the pinewood particles lost all features of
386 the parental structure, becoming spherical and porous with large inner cavi-
387 ties, formed from the simultaneous release of a large volatiles fraction. The
388 pinewood particles have undergone stronger melting during fast pyrolysis by
389 forming smooth and near-spherical structures. It is believed that under fast

390 heating the formation of metaplast is mostly affected by the bond-breaking
391 and cross-linking of organic components present in lignin that is less volatile
392 than holocelluloses. Surprisingly, beechwood char particles were only slightly
393 molten on the outer surface and kept the shape and size characteristics of
394 the parental fuel, contrary to the results of Dall’Ora et al [9].

395 This observation is most likely caused by the presence of beechwood
396 at a stage of being converted from the water-conducting sapwood to the
397 heartwood, and to formation of tyloses, which are filled with a large quantity
398 of phenolic compounds, lignin, and aromatic substances [49, 50]. The formed
399 phenolic compounds polymerize in insoluble forms, for example in a non-
400 lignin related bio-polymer suberin that makes the wood particle more stable
401 at high heat treatment temperatures [51, 52].

402 Alfalfa straw and wheat straw have underwent plasticization, but less
403 melting than the pinewood, indicating an effect of ash on the char morphol-
404 ogy. The high levels of K and Ca in the herbaceous biomasses could cause
405 less severe plasticization, by catalyzing the conversion of bridges into char
406 links, and therefore increasing polymerization / cross-linking and reducing
407 char fluidity. The alfalfa and wheat straw char obtained two types of a par-
408 ticle shape (elongated cylindrical and near-spherical). The transformation of
409 herbaceous char shapes was probably affected by the presence of potassium
410 and calcium silicates, remaining in the char. The high Ca content in the
411 alfalfa straw could provide additional stability to the char, preserving the
412 particle size of the original fuel.

413 In the present study, the effect of extractives on the char structural
414 transformations was studied by removing resin, fatty acids, waxes, and phy-

415 tosterols from the pinewood and beechwood by acetone extraction. Fig-
416 ure 10 shows the char structures of pinewood and beechwood. The pinewood
417 char after the extraction exhibited stronger swelling and enhanced sticking
418 of smaller particles to the surface of larger particles at 1000°C. The beech-
419 wood char without extractives showed slightly stronger melting than the
420 non-treated beechwood char. The extractives could affect the char fluidity.
421 The nearly similar levels of K and Ca in the char of non-treated and extracted
422 wood showed that the extraction process did not have an effect on biomass
423 ash content.

424 *Soot morphology.* In the fast DTF pyrolysis, the solid sub-micron particles
425 were collected on a filter. The particulate matter at 1250-1400°C was char-
426 acterized by TEM and SEM microscopy. The collected nano-sized particles
427 were spherical and attached to each other forming long chain-like structures.
428 Due to the near-spherical shape and particle size < 100 nm, the particulate
429 matter on the filter was identified as soot, mixed with inorganic matter as
430 shown in Figure 11.

431 Interestingly, also larger sub-micron particles of a size > 100 nm were
432 observed in the particulate matter. The wheat straw fast pyrolysis generated
433 larger sub-micron particles of size 100-300 nm, agglomerated with smaller
434 units of size 5-20 nm, while during the wood pyrolysis the particle size was
435 between 20 and 150 nm. The formation of particles of size between 60 nm and
436 300 nm at high temperatures during fast pyrolysis has not been extensively
437 discussed in the literature before. However, the differences in a carbon nano-
438 structure and graphitization degree may affect soot reactivity as mentioned
439 previously [43, 53].

440 4. Conclusion

441 Char yields from the DTF were lower than those obtained in a wire mesh
442 reactor. This was attributed to the higher heating rates in the DTF, while
443 self-gasification by reaction with CO₂ and H₂O was of minor importance.
444 The straw samples showed a significant char yield decrease in the DTF when
445 the temperature was increased from 1000 to 1400°C, whereas the char yields
446 of pinewood ($\approx 3.5\%$, daf) and beechwood ($\approx 7\%$, daf) were almost con-
447 stant at a very low level. It was observed that low fuel alkali content, high
448 temperatures, and fast heating rates lead to low biomass char yields. The
449 results indicated that the influence of alkali on the char yield is more pro-
450 nounced at low and intermediate heating rates than at fast heating rates in
451 the DTF.

452 The measured soot yield of wood was 3-7% higher compared to herba-
453 ceous biomass above 1250°C. Leaching of the wheat straw resulted in a re-
454 duction of the soot fraction, indicating that suppression of soot by a high
455 potassium content only plays a minor role. However, the higher concentra-
456 tion of lignin and resin acids in the wood could lead to a larger formation
457 of PAH precursors and thus higher soot yields. The lower soot yields in
458 pyrolysis of leached wheat straw compared to alfalfa straw and non-treated
459 wheat straw were related to the removal of organic compounds, and there-
460 fore decreased formation of PAH precursors. Significant levels of K, Cl and S
461 elements were found in the straw soot. The particle size of herbaceous soot
462 varied from 5 nm to 300 nm, whereas the wood formed particles from 20 nm
463 to 150 nm.

464 The pyrolysis process caused the characteristic length of both wood sam-

465 ples and wheat straw particles to decrease by a factor of two as shown by
466 2D dynamic imaging analysis, while the pinewood char obtained the most
467 spherical shape. The beechwood and herbaceous char particles retained a
468 cylindrical shape. Scanning electron microscopy on the chars indicated struc-
469 tural transformations of all biomass under fast heating. The chars underwent
470 strong deformation with clear signs of melting and development of macropo-
471 res at all applied temperatures. The ability of char to melt under the fast
472 heating followed the order pinewood > wheat straw, alfalfa straw > beech-
473 wood, and was related to the formation of a metaplast with a stronger con-
474 tribution of lignin due to its lower volatility and remaining high-temperature
475 stable extractives (suburin, tannin) in the beechwood char. In addition, a
476 significant catalytic effect of K and Ca on the fuel structural changes was
477 observed due to a stronger cross-linking of herbaceous chars, leading to less
478 fluidity. The increased melting of pinewood and beechwood could indicate
479 some influence of extractives on the char morphology.

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486 measurements.

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Table 1:

Fuel	Pine-wood	Beech-wood	Wheat straw	Alfalfa straw	Leached wheat straw	Pine-wood*	Beech wood*
Proximate analysis							
Moisture, (wt. % ar)	5.1	4.5	5.5	5.2	4.3	5.1	5.1
Ash (550°C), (wt. % db)	0.3	1.4	4.1	7.4	2	0.3	1.5
Volatiles, (wt. % db)	86.6	79.4	77.5	75.9	84.2	84.9	79.3
HHV, (MJ/kg)	21.6	20.2	18.8	19.7	18.7	20.3	20.3
LHV, (MJ/kg)	20.2	19	17.5	16.9	17.4	19	19
Ultimate analysis, (wt. % db)							
C	53.1	50.7	46.6	42.5	45.7	50.1	50
H	6.5	5.9	6.1	6.7	6.6	6	5.8
O	40	41.9	42.5	43.1	45.4	43.5	42.6
N	0.06	0.13	0.6	0.3	0.3	0.05	0.08
S	<0.01	0.02	0.1	0.03	0.02	0.008	0.019
Cl	0.01	0.02	0.1	0.5	0.01	0.005	0.02
Ash compositional analysis, (mg/kg, db)							
Al	10	10	150	600	100	8.3	15.9
Ca	600	2000	2500	12900	1300	620	2090
Fe	20	10	200	-	350	8	10
K	200	3600	11000	28000	1300	250	3700
Mg	100	600	750	1400	350	120	610
Na	30	100	150	1000	50	60	150
P	6	150	550	1900	80	25	120
Si	50	200	8500	2000	6200	33	200
Ti	2	8	10	30	10	1	4

*after extraction

Table 2:

Biomass	Cellulose	Hemi-cellulose	Lignin		Extractives	Protein
			acid in-soluble	acid soluble		
Pinewood	38.3	17.8	29.6	1.8	8.8*	0.6
Beechwood	35	19.2	32	1.5	7.5*	1.9
Wheat straw	35.9	18	19.2	6.5	10.1**	6.3
Leached wheat straw	32.1	23.5	13.8	2	13.3**	1.3
Alfalfa straw	18.8	12	14.7	6.8	39.6**	5.1

* acetone extraction ** ethanol-water extraction (room temperature)

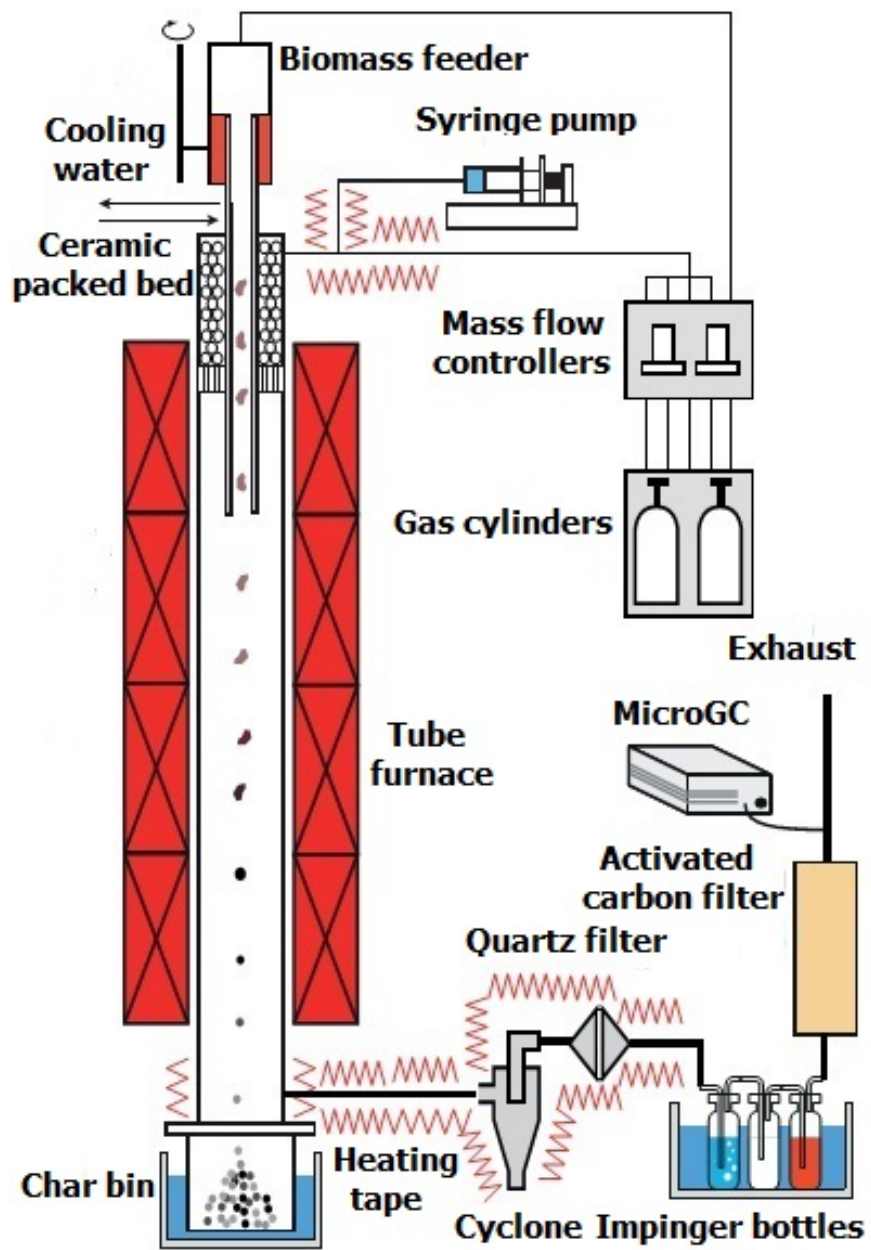
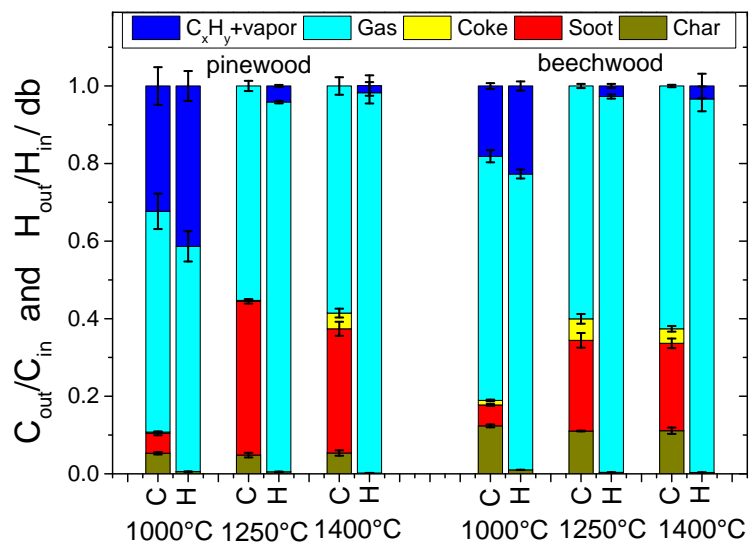
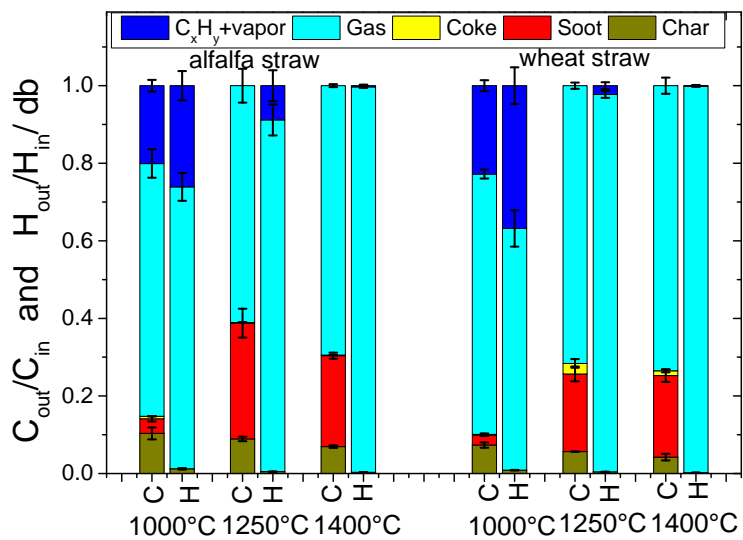


Figure 1

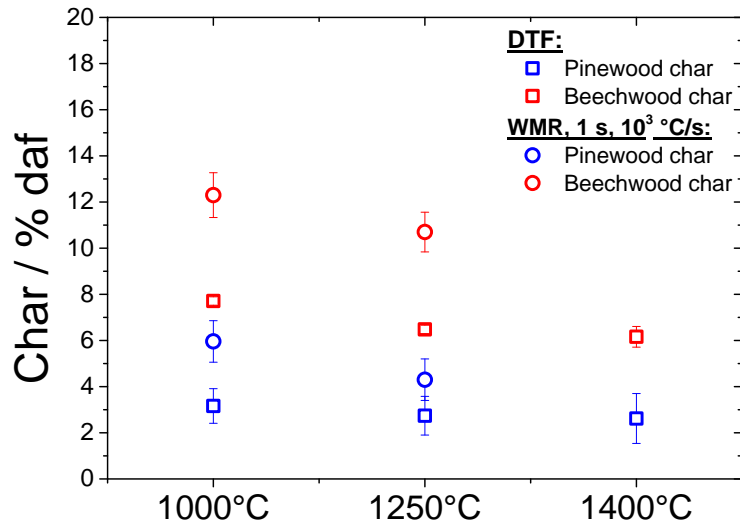


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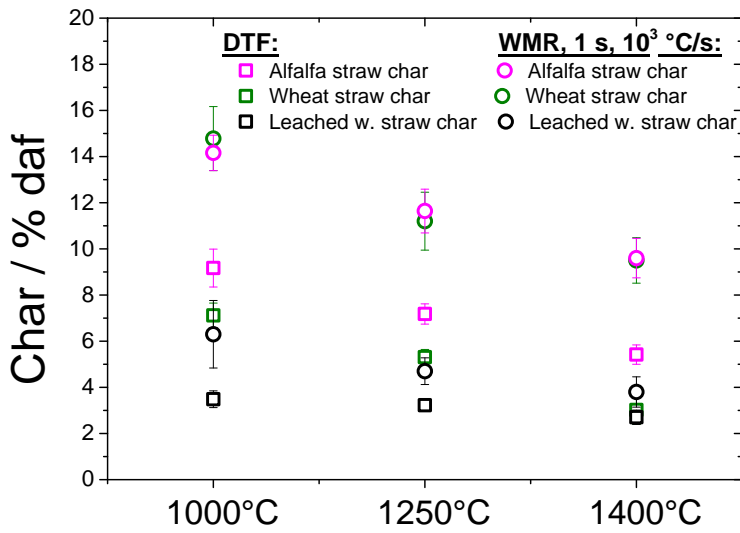


2.2:

Figure 2:

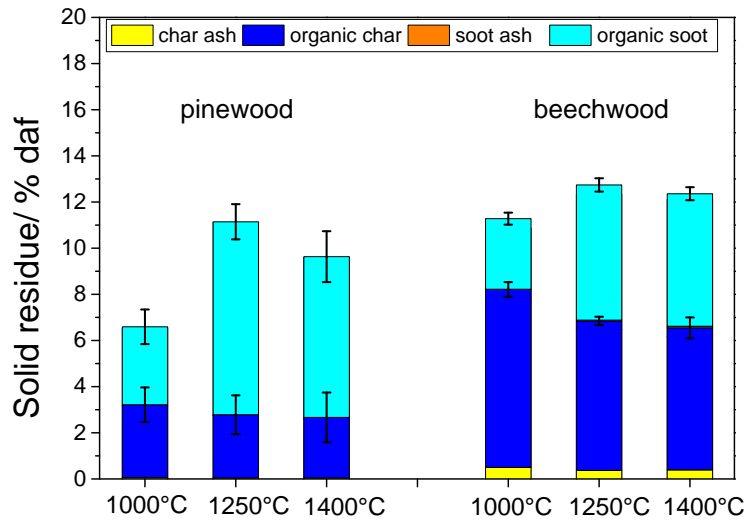


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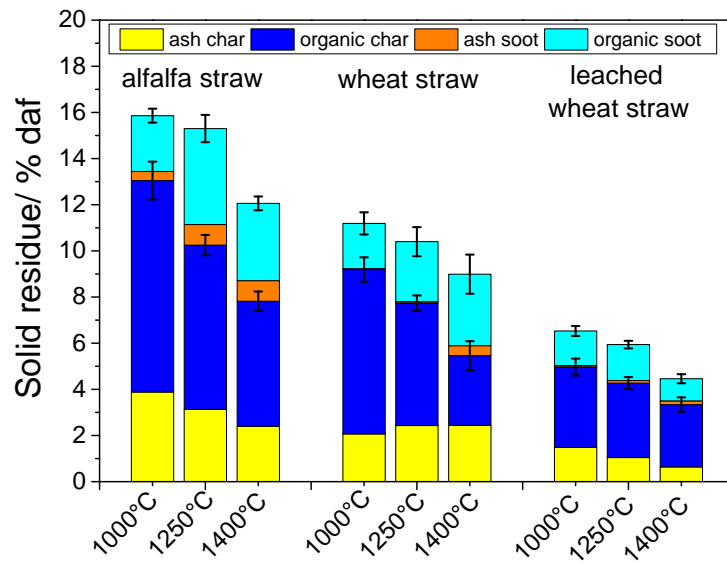


3.2:

Figure 3:

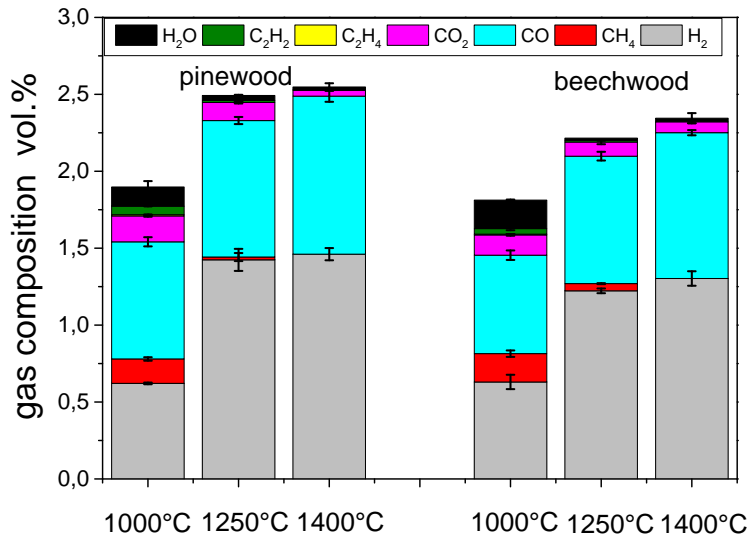


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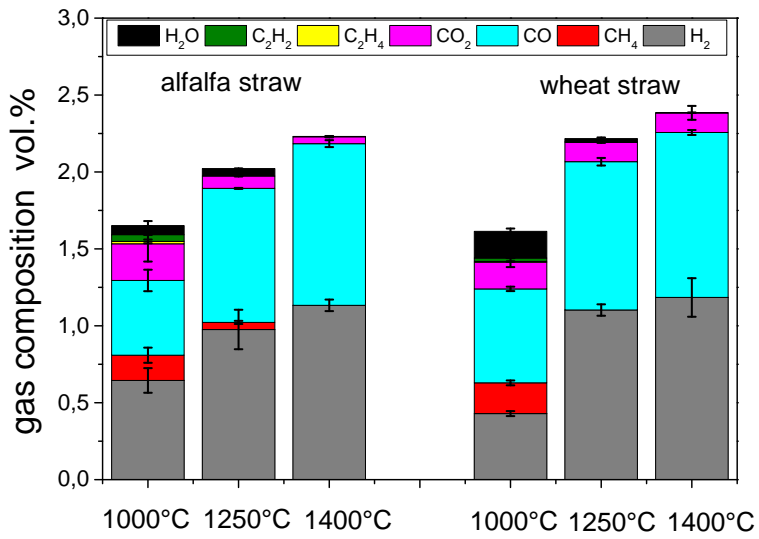


4.2:

Figure 4:



5.1:



5.2:

Figure 5:

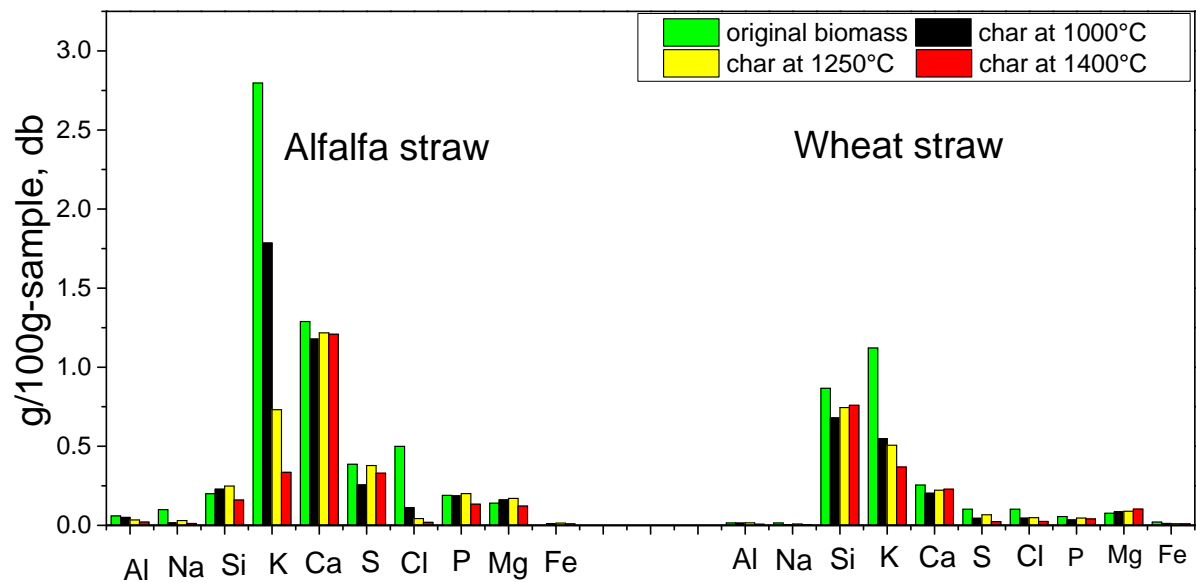


Figure 6

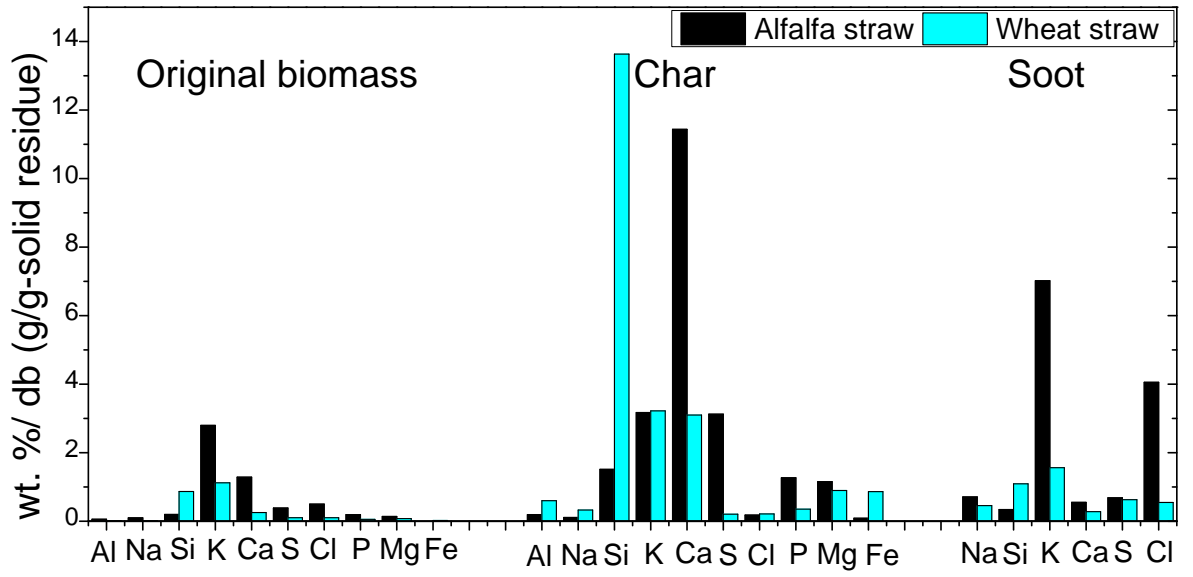
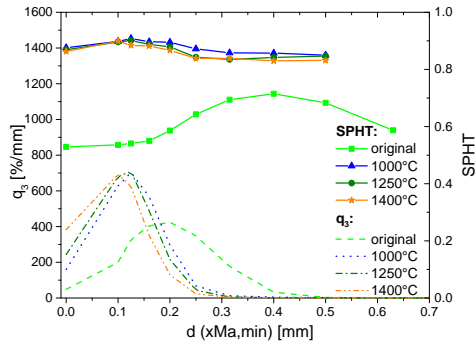
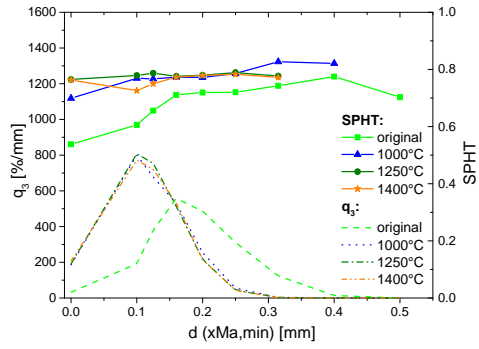


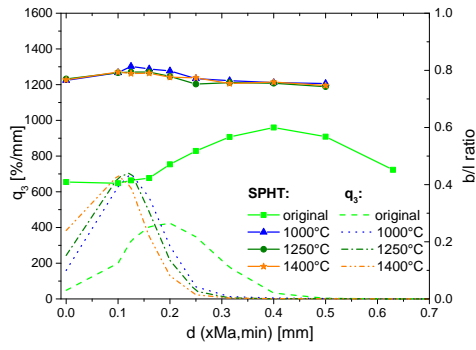
Figure 7



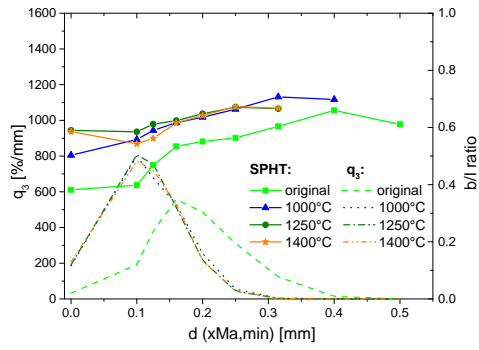
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8.2:

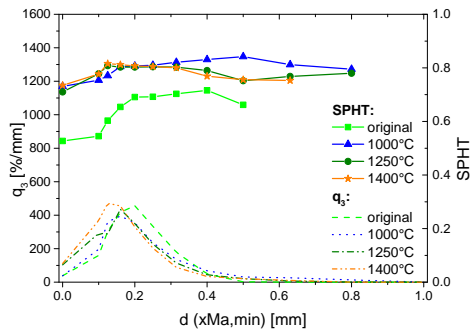


8.3:

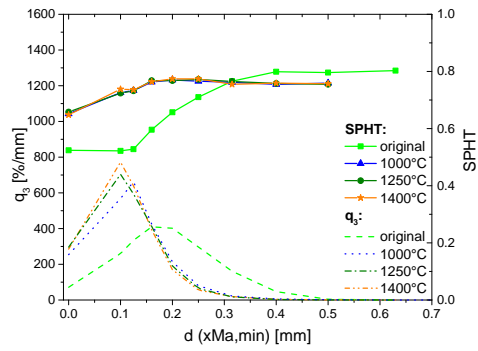


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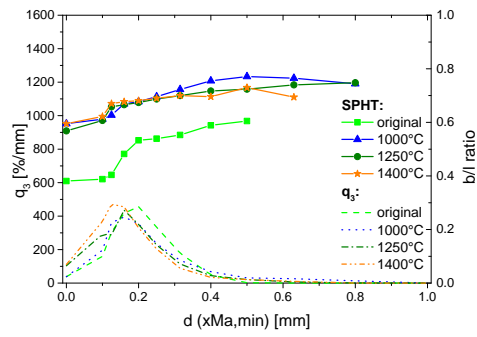
Figure 8:



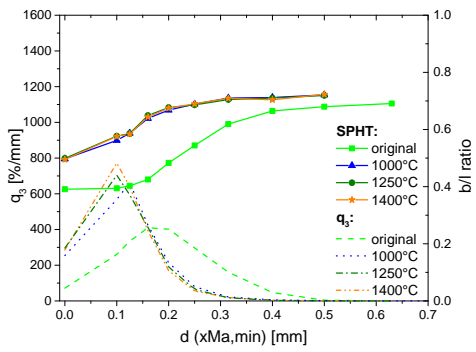
9.1:



9.2:

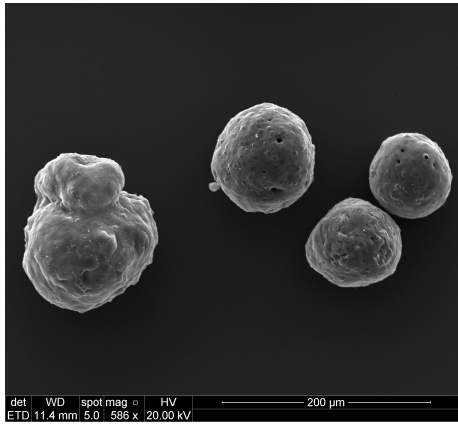


9.3:

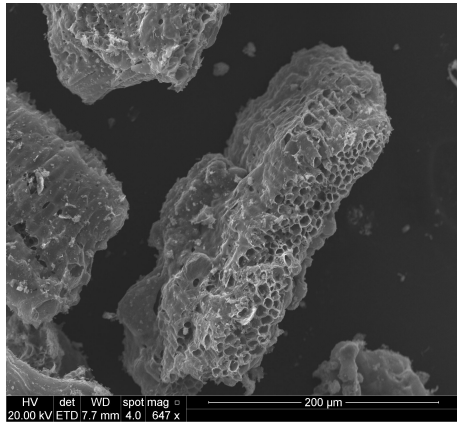


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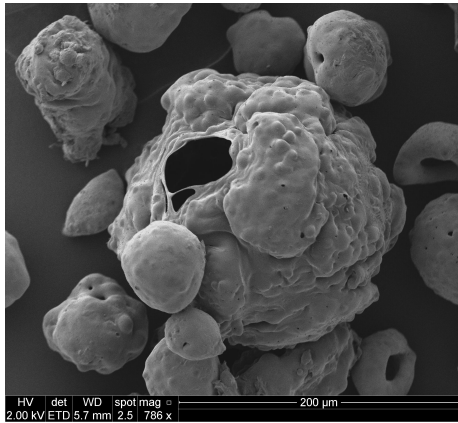
Figure 9:



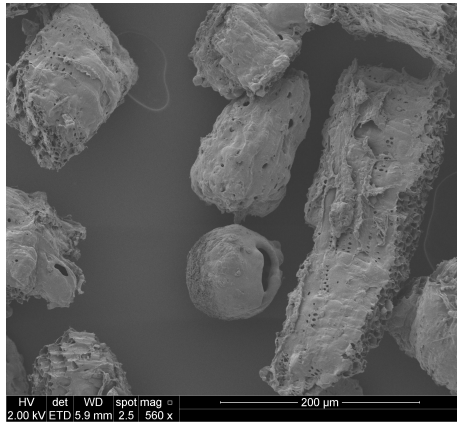
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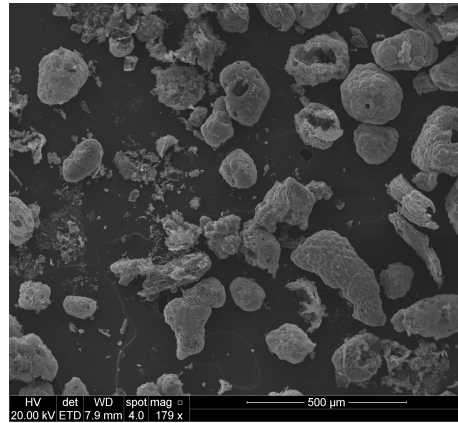
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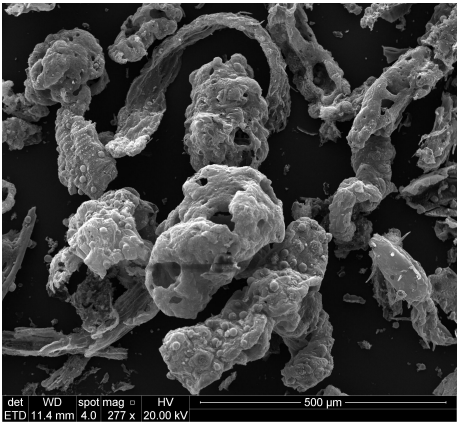
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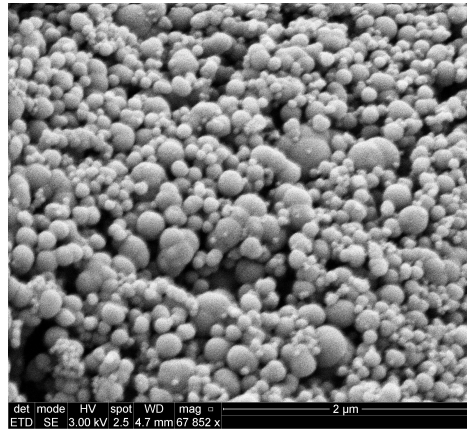


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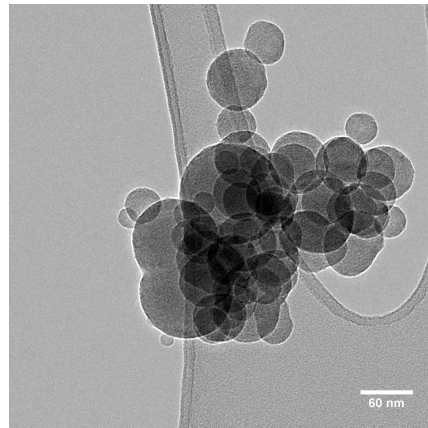


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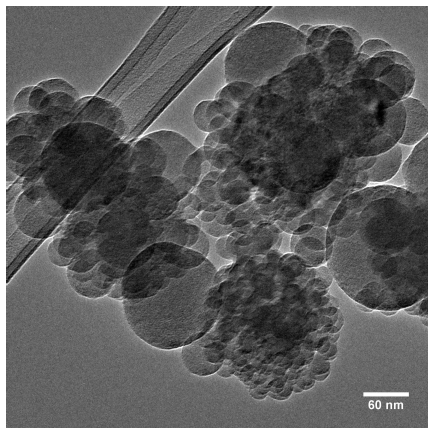
Figure 10:



11.1:



11.2:



11.3:

Figure 11:
42

Captions for tables and figures

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636

637 Table 1: Proximate, ultimate and ash analyses of fuels.

638 Table 2: Biomass feedstock composition, calculated in percentage based on
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656 rated in ash and organic matters. The error bars characterize the deviations
657 between the total yields of the char and soot.

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671 1250 and 1400°C.
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684 at 1000°C and compared with the pinewood and beechwood after extraction

685 with acetone, reacted at 1000°C, and alfalfa and wheat straw chars, reacted
686 at 1400°C. SEM images of alfalfa straw and wheat straw were taken under a
687 lower magnification to show at least two particles of a different shape in the
688 same image (elongated and near-spherical).

689 Figure 10.1: Pinewood

690 Figure 10.2: Beechwood

691 Figure 10.3: Pinewood ext.-free

692 Figure 10.4: Beechwood ext.-free

693 Figure 10.5: Alfalfa straw

694 Figure 10.6: Wheat straw

695 Figure 11: SEM image of pinewood soot, reacted at 1400°C; TEM of beech-
696 wood and alfalfa straw soot.

697 Figure 11.1: Pinewood

698 Figure 11.2: Beechwood

699 Figure 11.3: Alfalfa straw

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